

Dual, 8-/10-/12-/14-Bit Low Power Digital-to-Analog Converters AD9114/AD9115/AD9116/AD9117

FEATURES

Power dissipation @ 3.3 V, 20 mA output 191 mW @ 10 MSPS 232 mW @ 125 MSPS Sleep mode: <3 mW @ 3.3 V Supply voltage: 1.8 V to 3.3 V SFDR to Nyquist 86 dBc @ 1 MHz output 85 dBc @ 10 MHz output AD9117 NSD @ 1 MHz output, 125 MSPS, 20mA: −162 dBc/Hz Differential current outputs: 4 mA to 20 mA Two on-chip auxiliary DACs CMOS inputs with single-port operation Output common mode: adjustable 0 V to 1.2 V Small footprint 40-lead LFCSP Pb-free package

APPLICATIONS

Wireless infrastructures Picocell, femtocell base stations Medical instrumentation Ultrasound transducer excitation Portable instrumentation Signal generators, arbitrary waveform generators

GENERAL DESCRIPTION

The AD9114/AD9115/AD9116/AD9117 are pin-compatible dual, 8-/10-/12-/14-bit, low power digital-to-analog converters (DACs) that provide a sample rate of 125 MSPS. These TxDAC® converters are optimized for the transmit signal path of communication systems. All the devices share the same interface, LFCSP, and pinout, providing an upward or downward component selection path based on performance, resolution, and cost.

The AD9114/AD9115/AD9116/AD9117 offer exceptional ac and dc performance and support update rates up to 125 MSPS.

The flexible power supply operating range of 1.8 V to 3.6 V and low power dissipation of the AD9114/AD9115/AD9116/AD9117 make them well-suited for portable and low power applications.

PRODUCT HIGHLIGHTS

1. Low Power.

DACs operate on a single 1.8 V to 3.3 V supply; total power consumption reduces to 225 mW at 100 MSPS. Sleep and power-down modes are provided for low power idle periods.

- 2. CMOS Clock Input. High speed, single-ended CMOS clock input supports 125 MSPS conversion rate.
- 3. Easy Interfacing to Other Components. Adjustable output common mode from 0 V to 1.2 V allows for easy interfacing to other components that accept commonmode levels greater than 0 V.

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REVISION HISTORY

8/08—Revision 0: Initial Version

FUNCTIONAL BLOCK DIAGRAM

Figure 1.

SPECIFICATIONS

DC SPECIFICATIONS

 T_{MIN} to T_{MAX} , $AVDD = 3.3$ V, $DVDD = 1.8$ V, $DVDDIO = 3.3$ V, $CVDD = 3.3$ V, $I_{OUTFS} = 2$ mA, maximum sample rate, unless otherwise noted.

Table 1.

1 Based on a 10 kΩ external resistor.

DIGITAL SPECIFICATIONS

 T_{MIN} to T_{MAX} , AVDD = 3.3 V, DVDD = 1.8 V, DVDDIO = 3.3 V, CVDD = 3.3 V, Ioutrs = 2 mA, maximum sample rate, unless otherwise noted.

Table 2. Parameter Min Typ Max Unit DAC CLOCK INPUT (CLKIN) V_{IH} 2.1 3 mV $V_{I L}$ and $V_{I L$ Maximum Clock Rate **125 MSPS** MSPS **Maximum Clock Rate** 125 MSPS SERIAL PERIPHERAL INTERFACE Maximum Clock Rate (SCLK) 25 MHz Minimum Pulse Width High 20 ns and the United States of the United States o Minimum Pulse Width Low 20 ns INPUT DATA TIMING 1.8 V Q-Channel or DCLKIO Falling Edge Setup 0.25 ns Hold 1.2 ns I-Channel or DCLKIO Rising Edge Setup 0.13 ns Hold 1.1 ns 3.3 V Q-Channel or DCLKIO Falling Edge Setup −0.2 ns Hold the contract of the contr I-Channel or DCLKIO Rising Edge Setup −0.2 ns Hold the contract of the contr V_{IH} 2.1 3 | V $V_{I L}$ 0 0.9

AC SPECIFICATIONS

 T_{MIN} to T_{MAX} , AVDD = 3.3 V, DVDD = 1.8 V, DVDDIO = 1.8 V, CVDD = 3.3 V, I_{OUTFS} = 20 mA, maximum sample rate, unless otherwise noted.

Table 3.

 T_{MIN} to T_{MAX} , AVDD = 1.8 V, DVDD = 1.8 V, DVDDIO = 1.8 V, CVDD = 3.3 V, Ioutrs = 8 mA, maximum sample rate, unless otherwise noted.

Table 4.

ABSOLUTE MAXIMUM RATINGS

Table 5.

Stresses above those listed under Absolute Maximum Ratings may cause permanent damage to the device. This is a stress rating only; functional operation of the device at these or any other conditions above those indicated in the operational section of this specification is not implied. Exposure to absolute maximum rating conditions for extended periods may affect device reliability.

THERMAL RESISTANCE

Table 6.

ESD CAUTION

ESD (electrostatic discharge) sensitive device. Charged devices and circuit boards can discharge without detection. Although this product features patented or proprietary protection circuitry, damage may occur on devices subjected to high energy ESD. Therefore, proper ESD precautions should be taken to avoid performance degradation or loss of functionality.

Figure 2. AD9117 Pin Configuration

Table 7. AD9117 Pin Function Descriptions

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Table 8. AD9116 Pin Function Descriptions

Figure 4. AD9115 Pin Configuration

TYPICAL PERFORMANCE CHARACTERISTICS

AVDD, DVDD, DVDDIO, CVDD = 1.8 V, IouTFS = 8 mA, maximum sample rate (125 MSPS), unless otherwise noted.

Figure 41. AD9117 1-Carrier W-CDMA First Adjacent Channel ACLR 1.8 V

Figure 42. AD9117 1-Carrier W-CDMA Second Adjacent Channel ACLR 1.8 V

Figure 43. AD9117 1-Carrier W-CDMA Third Adjacent Channel ACLR 1.8 V

Figure 44. AD9117 1-Carrier W-CDMA Third Adjacent Channel ACLR 3.3 V

Figure 45. AD9117 1-Carrier W-CDMA Second Adjacent Channel ACLR 3.3 V

Figure 46. AD9117 1-Carrier W-CDMA Third Adjacent Channel ACLR 3.3 V

Figure 47. AD9117 2-Carrier W-CDMA First Adjacent Channel ACLR 1.8 V

Figure 48. AD9117 2-Carrier W-CDMA Second Adjacent Channel ACLR 1.8 V

Figure 49. AD9117 2-Carrier W-CDMA Third Adjacent Channel ACLR 1.8 V

Figure 50. AD9117 2-Carrier W-CDMA First Adjacent Channel ACLR 3.3 V

Figure 51. AD9117 2-Carrier W-CDMA Second Adjacent Channel ACLR 3.3 V

Figure 52. AD9117 2-Carrier W-CDMA Third Adjacent Channel ACLR 3.3 V

Figure 53. IMD at Three Digital Signal Levels, 1.8 V

Figure 56. IMD Over Temperature at 8 mA, 1.8 V

Figure 59. SFDR vs. Digital Signal Level 3.3 V

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07466-088

07466-089

07466-089

TERMINOLOGY

Linearity Error or Integral Nonlinearity (INL)

Linearity error is defined as the maximum deviation of the actual analog output from the ideal output, determined by a straight line drawn from zero scale to full scale.

Differential Nonlinearity (DNL)

DNL is the measure of the variation in analog value, normalized to full scale, associated with a 1 LSB change in digital input code.

Monotonicity

A DAC is monotonic if the output either increases or remains constant as the digital input increases.

Offset Error

Offset error is the deviation of the output current from the ideal of zero. For I_{OUTP}, 0 mA output is expected when the inputs are all 0. For I_{OUTN}, 0 mA output is expected when all inputs are set to 1.

Gain Error

Gain error is the difference between the actual and ideal output span. The actual span is determined by the difference between the output when all inputs are set to 1 and the output when all inputs are set to 0.

Output Compliance Range

Output compliant range is the range of allowable voltage at the output of a current-output DAC. Operation beyond the maximum compliance limits can cause either output stage saturation or breakdown, resulting in nonlinear performance.

Temperature Drift

Temperature drift is specified as the maximum change from the ambient value (25 $^{\circ}$ C) to the value at either T_{MIN} or T_{MAX} . For offset and gain drift, the drift is reported in ppm of fullscale range per degree Celsius (ppm FSR/°C). For reference drift, the drift is reported in parts per million per degree Celsius (ppm/°C).

Power Supply Rejection

Power supply rejection is the maximum change in the full-scale output as the supplies are varied from minimum to maximum specified voltages.

Settling Time

Settling time is the time required for the output to reach and remain within a specified error band around its final value, measured from the start of the output transition.

Spurious Free Dynamic Range (SFDR)

SFDR is the difference, in decibels (dB), between the peak amplitude of the output signal and the peak spurious signal between dc and the frequency equal to half the input data rate.

Total Harmonic Distortion (THD)

THD is the ratio of the rms sum of the first six harmonic components to the rms value of the measured fundamental. It is expressed as a percentage (%)or in decibels (dB).

Signal-to-Noise Ratio (SNR)

SNR is the ratio of the rms value of the measured output signal to the rms sum of all other spectral components below the Nyquist frequency, excluding the first six harmonics and dc. The value for SNR is expressed in decibels.

Adjacent Channel Leakage Ratio (ACLR)

ACLR is the ratio in decibels relative to the carrier (dBc) between the measured power within a channel relative to its adjacent channel.

Complex Image Rejection

In a traditional two-part upconversion, two images are created around the second IF frequency. These images have the effect of wasting transmitter power and system bandwidth. By placing the real part of a second complex modulator in series with the first complex modulator, either the upper or lower frequency image near the second IF can be rejected.

THEORY OF OPERATION

Figure 75. Simplified Block Diagram

[Figure 75](#page-29-1) shows a simplified block diagram of the AD9114/ AD9115/AD9116/AD9117 that consists of two main DACs, digital control logic, and a full-scale output current control. The DAC contains a PMOS current source array capable of providing a maximum of 20 mA. The array is divided into 31 equal currents that make up the five most significant bits (MSBs). The next four bits, or middle bits, consist of 15 equal current sources whose value is 1/16 of an MSB current source. The remaining LSBs are binary weighted fractions of the current sources of the middle bits. Implementing the middle and lower bits with current sources, instead of an R-2R ladder, enhances its dynamic performance for multitone or low amplitude signals and helps maintain the high output impedance of the DAC (that is, >200 MΩ).

All of these current sources are switched to one or the other of the two output nodes (IOUTP or IOUTN) via PMOS differential current switches. The switches are based on the architecture that was pioneered in the AD976x family, with further refinements to reduce distortion contributed by the switching transient. This switch architecture also reduces various timing errors and provides matching complementary drive signals to the inputs of the differential current switches.

The analog and digital sections of the AD9114/AD9115/AD9116/ AD9117 have separate power supply inputs (AVDD and DVDD) that can operate independently over a 1.7 V to 3.5 V range. The digital section, which is capable of operating at a rate of up to 125 MSPS, consists of edge-triggered latches and segment decoding logic circuitry. The analog section includes the PMOS current sources, the associated differential switches, a 1.0 V band gap voltage reference, and a reference control amplifier.

Each DAC full-scale output current is regulated by the reference control amplifier and can be set from 4 mA to 20 mA via an external resistor, RSET, connected to its full-scale adjust pin (FSADJ).

The external resistor, in combination with both the reference control amplifier and voltage reference, V_{REFO} , sets the reference current, IREF, which is replicated to the segmented current sources with the proper scaling factor. The full-scale current, I_{OUTFS}, is $32 \times I_{REF}$.

Optional on-chip RSET resistors are provided that can be programmed between an nominal value of 1.5 kΩ to 8.5 kΩ $(4 \text{ mA to } 20 \text{ mA}$ I_{OUTFS}).

The AD9114/AD9115/AD9116/AD9117 provide the option of setting the output common mode to a value other than ACOM via the output common-mode pin (CMLI). This facilitates directly interfacing the output of the AD9114/AD9115/ AD9116/AD9117 to components that require common-mode levels greater than 0 V.

SERIAL PERIPHERAL INTERFACE (SPI)

The serial port of the AD9114/AD9115/AD9116/AD9117 is a flexible, synchronous serial communications port allowing easy interfacing to many industry-standard microcontrollers and microprocessors. The serial I/O is compatible with most synchronous transfer formats, including both the Motorola SPI® and Intel® SSR protocols. The interface allows read/write access to all registers that configure the AD9114/AD9115/AD9116/AD9117. Single or multiple byte transfers are supported, as well as MSB first or LSB first transfer formats. The serial interface port of the AD9114/ AD9115/AD9116/AD9117 is configured as a single I/O pin on the SDIO pin.

GENERAL OPERATION OF THE SERIAL INTERFACE

There are two phases to a communication cycle on the AD9114/ AD9115/AD9116/AD9117. Phase 1 is the instruction cycle, which is the writing of an instruction byte into the AD9114/AD9115/ AD9116/AD9117, coinciding with the first eight SCLK rising edges. In Phase 2, the instruction byte provides the serial port controller of the AD9114/AD9115/AD9116/AD9117 with information regarding the data transfer cycle. The Phase 1 instruction byte defines whether the upcoming data transfer is a read or write, the number of bytes in the data transfer, and the starting register address for the first byte of the data transfer. The first eight SCLK rising edges of each communication cycle are used to write the instruction byte into the AD9114/AD9115/AD9116/AD9117.

A Logic 1 on Pin 35 (RESET/PINMD), followed by a Logic 0, resets the SPI port timing to the initial state of the instruction cycle. This is true regardless of the present state of the internal registers or the other signal levels present at the inputs to the SPI port. If the SPI port is in the midst of an instruction cycle or a data transfer cycle, none of the present data is written.

The remaining SCLK edges are for Phase 2 of the communication cycle. Phase 2 is the actual data transfer between the AD9114/ AD9115/AD9116/AD9117 and the system controller. Phase 2 of the communication cycle is a transfer of one, two, three, or four data bytes, as determined by the instruction byte. Using one multibyte transfer is the preferred method. Single byte data transfers are useful to reduce CPU overhead when register access requires one byte only. Registers change immediately upon writing to the last bit of each transfer byte.

INSTRUCTION BYTE

Table 11.

The instruction byte contains the information shown in Table 11.

 R/\overline{W} (Bit 7 of the instruction byte) determines whether a read or a write data transfer occurs after the instruction byte write. Logic 1 indicates a read operation. Logic 0 indicates a write operation. N1 and N0 (Bit 6 and Bit 5 of the instruction byte) determine the number of bytes to be transferred during the data transfer cycle. The bit decodes are shown in Table 12.

Table 12. Byte Transfer Count

A4, A3, A2, A1, and A0 (Bit 4, Bit 3, Bit 2, Bit 1, and Bit 0 of the instruction byte) determine which register is accessed during the data transfer portion of the communications cycle. For multibyte transfers, this address is the starting byte address. The remaining register addresses are generated by the AD9114/ AD9115/AD9116/AD9117, based on the LSBFIRST bit (Register 0x00, Bit 6).

SERIAL INTERFACE PORT PIN DESCRIPTIONS SCLK—Serial Clock

The serial clock pin is used to synchronize data to and from the AD9114/AD9115/AD9116/AD9117 and to run the internal state machines. The SCLK maximum frequency is 20 MHz. All data input to the AD9114/AD9115/AD9116/AD9117 is registered on the rising edge of SCLK. All data is driven out of the AD9114/ AD9115/AD9116/AD9117 on the falling edge of SCLK.

CS—Chip Select

An active low input starts and gates a communication cycle. It allows more than one device to be used on the same serial communications lines. The SDIO/FORMAT pin reaches a high impedance state when this input is high. Chip select should stay low during the entire communication cycle.

SDIO—Serial Data I/O

The SDIO pin is used as a bidirectional data line to transmit and receive data.

MSB/LSB TRANSFERS

The serial port of the AD9114/AD9115/AD9116/AD9117 can support both most significant bit (MSB) first or least significant bit (LSB) first data formats. This functionality is controlled by the LSBFIRST bit (Register 0x00, Bit 6). The default is MSB first $(LSBFIRST = 0)$.

When $LSBFIRST = 0$ (MSB first), the instruction and data bytes must be written from the most significant bit to the least significant bit. Multibyte data transfers in MSB first format start with an instruction byte that includes the register address of the most significant data byte. Subsequent data bytes should follow in order from a high address to a low address. In MSB first mode, the serial port internal byte address generator decrements for each data byte of the multibyte communications cycle.

When $LSBFIRST = 1$ (LSB first), the instruction and data bytes must be written from the least significant bit to the most significant bit. Multibyte data transfers in LSB first format start with an instruction byte that includes the register address of the least significant data byte followed by multiple data bytes. The serial port internal byte address generator increments for each byte of the multibyte communication cycle.

The serial port controller data address of the AD9114/AD9115/ AD9116/AD9117 decrements from the data address written toward 0x00 for multibyte I/O operations if the MSB first mode is active. The serial port controller address increments from the data address written toward 0x1F for multibyte I/O operations if the LSB first mode is active.

SERIAL PORT OPERATION

The serial port configuration of the AD9114/AD9115/AD9116/ AD9117 is controlled by Register 0x00. It is important to note that the configuration changes immediately upon writing to the last bit of the register. For multibyte transfers, writing to this register can occur during the middle of the communications cycle. Care must be taken to compensate for this new configuration for the remaining bytes of the current communications cycle.

The same considerations apply to setting the software reset, RESET (Register 0x00, Bit 5). All registers are set to their default values except Register 0x00, which remains unchanged.

Use of single-byte transfers or initiating a software reset is recommended when changing serial port configurations to prevent unexpected device behavior.

PIN MODE

The AD9114/AD9115/AD9116/AD9117 can also be operated without ever writing to the serial port. With RESET/PINMD (Pin 35) tied high, the SCLK pin becomes CLKMD to provide for clock mode control (see the [Retimer](#page-37-0) section), the SDIO pin becomes FORMAT and selects the input data format, and the former \overline{CS} pin serves to power down the device.

Operation is otherwise exactly as defined by the default register values in [Table 14](#page-33-1), so external resistors at FSADJI and FSADJQ are needed to set the DAC currents, and both DACs are active. This is also a convenient quick checkout mode.

DAC currents can be externally adjusted in pin mode by sourcing or sinking currents at the FSADJI/AUXI and FASDJQ/AUXQ pins as desired with the fixed resistors installed. An op amp output with appropriate series resistance would be one of many possibilities. This has the same effect as changing the resistor value. Place at least 10 kΩ resistors in series right at the DAC to guard against accidental short circuits and noise modulation. The REFIO pin can be adjusted ±25% in a similar manner, if desired.

SPI REGISTER MAP

Table 13.

SPI REGISTER DESCRIPTIONS

Reading these registers returns previously written values for all defined register bits, unless otherwise noted.

DIGITAL INTERFACE OPERATION

Digital data for the I and Q DACs is supplied over a single parallel bus (DB[MSB:0]) accompanied by a qualifying clock (DCLKIO). The I and Q data is provided to the chip in an interleaved double data rate (DDR) format. The maximum guaranteed data rate is 250 MSPS with a 125 MHz clock. The order of data pairing and the sampling edge selection is user programmable using the IFIRST and IRISING configuration bits, resulting in four possible timing diagrams. These are shown in [Figure 76](#page-36-1), [Figure 77](#page-36-2), [Figure 78](#page-36-3), and [Figure 79.](#page-36-4)

Ideally, the rising and falling edges of the clock fall in the center of the keep-in-window formed by the set-up and hold times, ts and t_H. Refer to [Table 2 fo](#page-5-1)r set-up and hold times. A detailed timing diagram is shown in [Figure 80](#page-36-5).

Figure 80. Set-Up and Hold Times for All Input Modes

In addition to the different timing modes listed i[n Table 2, t](#page-5-1)he input data can also be presented to the device in either unsigned binary or twos complement format. The format type is chosen via the TWOS configuration bit.

Figure 81. Simplified Diagram of AD9114/AD9115/AD9116/AD9117 Timing

DIGITAL DATA LATCHING AND RETIMER SECTION

The AD9114/AD9115/AD9116/AD9117 have two clock inputs, DCLKIO and CLKIN. The CLKIN is the analog clock whose jitter affects DAC performance, and the DCLKIO is a digital clock, probably from an FPGA that needs to have a fixed relationship with the input data to ensure that the data is picked up correctly by the flip-flops on the pads.

[Figure 81](#page-37-1) is a simplified diagram of the entire data capture system in the AD9114/AD9115/AD9116/AD9117. The double data rate input data, DB[13:0], is latched at the pads/pins either on the rising edge or the falling edge of the DCLKIO-INT clock, as determined by IRISING, the SPI bit. IFIRST, the SPI bit, determines which channel data is latched first (that is, I or Q). The captured data is then retimed to the internal clock (CLKIN-INT) in the retimer block before being sent to the final analog DAC core (D-FF (4)), which controls the current steering output switches. All delay blocks depicted in [Figure 81](#page-37-1) are noninverting, and any wires without an explicit delay block can be assumed to have no delay for the purpose of understanding.

Only one channel is shown in [Figure 81](#page-37-1) with the DATA pads (DB[13:0]) serving as double data rate pads for both channels.

The default PINMD and SPI settings are IE = high (closed) and OE = low (open). These settings are enabled when RESET/PINMD (Pin 35) is held high. In this mode, the user has to supply both DCLKIO and CLKIN. In PINMD, it is also recommended that the DCLKIO and the CLKIN be in-phase for proper functioning of the DAC, which can easily be ensured by tying the pins together on the PCB. If the user can access the SPI, settling IE low (that is, IE is high) causes the CLKIN to be used as the DCLKIO also.

Settling OE high in the SPI allows the user to get a DCLKIO output from the CLKIN input for use in the user's PCB system. It is strongly recommended that $IE = OE = high$ not be used even though the device may appear to function correctly.

Retimer

The AD9114/AD9115/AD9116/AD9117 have an internal data retimer circuit that compares the CLKIN-INT and DCLKIO-INT clocks and, depending on their phase relationship, selects a retimer clock (RETIMER-CLK) to safely transfer data from the DCLKIO used at the chip's input interface to the CLKIN used to clock the analog DAC cores (D-FF (4)).

The retimer selects one of the three phases shown in [Figure 82](#page-37-2). The retimer is controlled by the SPI bits is shown i[n Table 15.](#page-38-0)

Note that in most cases, more than one retimer phase works, and in such cases, the retimer arbitrarily picks one phase that works. The retimer cannot pick the best or safest phase. If the user has a working knowledge of the exact phase relationship between DCLKIO and CLKIN (and thus DCLKIO-INT and CLKIN-INT, because the delay is approximately the same for both clocks and equal to DELAY1), then the retimer can be forced to this phase with CLKMODEN = 1 as described in [Table 15 a](#page-38-0)nd the following paragraphs.

Table 15. Timer Register List

Table 16. CLKMODE Details

When reset is pulsed high and then returns low (the part is in SPI mode), the retimer runs and automatically selects a suitable clock phase for the RETIMER-CLK within 128 clock cycles. The SPI searching bit returns to low, indicating that the retimer has locked and the part is ready for use. The reacquire bit can be used to reinitiate phase detection in the I and Q retimers at any time. CLKMODEQ[1:0] and CLKMODEI[1:0] provide readback for the values picked by the internal phase detectors in the retimer (see [Table 16](#page-38-1)).

To force the two retimers (I and Q) to pick a particular phase for the retimer clock (they must both be forced to the same value), CLKMODEN should be set high and the required phase value is written into CLKMODEI[1:0]. For example, if the DCLKIO and the CLKIN are in phase to first order, the user could safely force the retimers to pick Phase 2 for the RETIMER-CLK. This forcing function may be useful for synchronizing multiple devices.

In pin mode, it is expected that the user tie CLKIN and DCLKIO together. The device has a small amount of programmable functionality using the now unused SPI pins (SCLK, SDIO, and CS). If the two chip clocks are tied together, the SCLK pin can be tied to ground and the chip uses a clock for the retimer that is 180° out of phase with the two input clocks (that is, Phase 2, which is the safest or best option). The chip has an additional option in pin mode when the redefined SCLK pin is high. Use this mode if utilizing pin mode, but CLKIN and DCLKIO are

not tied together (that is, not in phase). Holding SCLK high causes the internal clock detector to use the phase detector output to determine which clock to use in the retimer (that is, select a suitable RETIMER-CLK phase). The action of taking SCLK high causes the internal phase detector to reexamine the two clocks, and determine the relative phase. Whenever the user wants to reevaluate the relative phase of the two clocks the SCLK pin can be taken low and then high again.

ESTIMATING THE OVERALL DAC PIPELINE DELAY

DAC pipeline latency is affected by the phase of the RETIMER-CLK that is selected. If latency is critical to the system and needs to be constant, the retimer should be forced to a particular phase and not be allowed to automatically select a phase each time.

Consider the case when DCLKIO = CLKIN (that is, in phase), and the RETIMER-CLK is forced to Phase 2. Assume that IRISING is 1 (that is, I data is latched on the rising edge and Q data on the falling edge). Then the latency to the output for the I-channel is 3 clock cycles (D-FF (1), D-FF (3), and D-FF (4), but not D-FF (2) because it is latched on the half clock cycle or 180°). The latency to the output for the Q-channel from the time the falling edge latches it at the pads in D-FF (0) is 2.5 clock cycles (½ clock cycle to D-FF (1), 1 clock cycle to D-FF (3), and 1 clock cycle to D-FF (4)). This latency for the AD9114/ AD9115/AD9116/ AD9117 is case specific and needs to be calculated based on the RETIMER-CLK phase that is automatically selected or manually forced.

SELF-CALIBRATION

The AD9114/AD9115/AD9116/AD9117 have a self-calibration feature that improves the DNL of the device. Performing a selfcalibration on the device improves device performance in low frequency applications. The device performance in applications where the analog output frequencies are above 5 MHz are generally influenced more by dynamic device behavior than by DNL, and in these cases, self-calibration is unlikely to produce measurable benefits. The calibration clock frequency is equal to the DAC clock divided by the division factor chosen by the DIVSEL value. Each calibration clock cycle is between 32 and 2048 DAC input clock cycles, depending on the value of DIVSEL[2:0] (Register 0x0E, Bits[2:0]). The frequency of the calibration clock should be between 0.5 MHz and 4 MHz for reliable calibrations. Best results are obtained by setting DIVSEL[2:0] (Register 0x0E, Bits[2:0]) to produce a calibration clock frequency between these values. Separate self-calibration hardware is included for each DAC. The DACs can be self-calibrated individually or simultaneously.

To perform a device self-calibration, the following procedure can be used:

- 1. Write 0x00 to Register 0x12. This ensures that the UNCALI and UNCALQ bits are reset.
- 2. Set up a calibration clock between 0.5 MHz and 4 MHz using DIVSEL[2:0], and then enable the calibration clock by setting the CALCLK bit (Register 0x0E, Bit 3).
- 3. Select the DAC(s) to self-calibrate by setting either Bit 4 (CALSELI) for the I DAC and/or Bit 5 (CALSELQ) for the Q DAC in Register 0x0E. Note that each DAC contains independent calibration hardware so they can be calibrated simultaneously.
- 4. Start self-calibration by setting Bit 4 in Register 0x12. Wait approximately 300 calibration clock cycles.
- 5. Check if the self-calibration has completed by reading the CALSTATI bit (Bit 6) and CALSTATQ bit (Bit 7) in Register 0x0F. Logic 1 indicates the calibration has completed.
- 6. When the self-calibration has completed, write 0x00 to Register 0x12.
- 7. Disable the calibration clock by clearing the CALCLK bit (Register 0x0E, Bit 3).

The AD9114/AD9115/AD9116/AD9117 allow reading and writing of the calibration coefficients. There are 32 coefficients in total. The read/write feature of the coefficients can be useful for improving the results of the self-calibration routine by averaging the results of several self-calibration cycles and loading the averaged results back into the device.

To read the calibration coefficients, use the following steps:

- 1. Select which DAC core to read by setting either Bit 4 (CALSELI) for the I DAC and/or Bit 5 (CALSELQ) for the Q DAC in Register 0x0E. Write the address of the first coefficient (0x01) to Register 0x10.
- 2. Set the SMEMRD bit (Register 0x12, Bit 2) by writing 0x04 to Register 0x12.
- 3. Read the 6-bit value of the first coefficient by reading the contents of Register 0x11.
- 4. Clear the SMEMRD bit by writing 0x00 to Register 0x12.
- 5. Repeat Step 2 through Step 4 for each of the remaining 31 coefficients by incrementing the address by one for each read.
- 6. Deselect the DAC core by clearing either Bit 4 (CALSELI) for the I DAC and/or Bit 5 (CALSELQ) for the Q DAC in Register 0x0E.

To write the calibration coefficients to the device, use the following steps:

- 1. Select which DAC core to read by setting either Bit 4 (CALSELI) for the I DAC and/or Bit 5 (CALSELQ) for the Q DAC in Register 0x0E.
- 2. Set the SMEMWR bit (Register 0x12, Bit 3) by writing 0x08 to Register 0x12.
- 3. Write the address of the first coefficient (0x01) to Register 0x10.
- 4. Write the value of the first coefficient to Register 0x11.
- 5. Repeat Step 2 through Step 4 for each of the remaining 31 coefficients by incrementing the address by one for each write.
- 6. Clear the SMEMWR bit by writing 0x00 to Register 0x12.
- 7. Deselect the DAC core by clearing either Bit 4 (CALSELI) for the I DAC and/or Bit 5 (CALSELQ) for the Q DAC in Register 0x0E.

COARSE GAIN ADJUSTMENT

Option 1

A coarse full-scale output current adjustment can be achieved using the lower six bits in Register 0x0D. This adds or subtracts up to 20% from the band gap voltage on Pin 34 (REFIO), and the voltage on the FSADJx resistors tracks this change. As a result, the DAC full-scale current varies the same amount. A secondary effect to changing the REFIO voltage is that the full-scale voltage in the AUXDAC also changes by the same magnitude. The register uses twos complement format, in which 011111 maximizes the voltage on the REFIO node and 100000 minimizes the voltage.

Option 2

While utilizing the internal FSADJx resistors, each main DAC can achieve independently controlled coarse gain using the lower six bits of Register 0x04 (IRSET[5:0]) and Register 0x07 (QRSET[5:0]). Unlike Coarse Gain Option 1, this impacts only the main DAC full-scale output current. The register uses twos complement format and allows the output current to be changed in approximately 0.25 dB steps.

Option 3

Even when the device is in pin mode, full-scale values can be adjusted by sourcing or sinking current from the FSADJ pins. Any noise injected here appears as amplitude modulation of the output. Thus, a portion of the required series resistance (at least 20 kΩ) must be installed right at the pin. A range of $±10\%$ is quite practical using this method.

Option 4

As in Option 3, when the device is in pin mode both full-scale values can be adjusted by sourcing or sinking current from the REFIO pin. Noise injected here appears as amplitude modulation of the output, so a portion of the required series resistance (at least 10 k Ω) must be installed at the pin. A range of ±25% is quite practical when using this method.

Fine Gain

Each main DAC has independent fine gain control using the lower six bits in Register 0x03 (I DAC gain) and Register 0x06 (Q DAC gain). Unlike Coarse Gain Option 1, this impacts only the main DAC full-scale output current. This register uses straight binary format. One application where straight binary format is critical is for side-band suppression while using a quadrature modulator. This is described in more detail in the [Applications](#page-42-2) [Information](#page-42-2) section.

USING THE INTERNAL TERMINATION RESISTORS

The AD9117/AD9116/AD9115/AD9114 have four 62.5 Ω termination internal resistors (two for each DAC output). To use these resistors to convert the DAC output current to a voltage, connect each DAC output pin to the adjacent load pin. For example, on the I DAC, IOUTP must be shorted to RLIP and IOUTN must be shorted to RLIN. In addition, the CMLI or CMLQ pin must be connected to ground directly or through a resistor. If the output current is at the nominal 20 mA and the CMLI or CMLQ pin is tied directly to ground, this produces a dc common-mode bias voltage on the DAC output equal to 0.5 V. If the DAC dc bias needs to be higher than 0.5 V, an external resistor can be connected between the CMLI or CMLQ pin and ground. This part also has an internal common-mode resistor that can be enabled. This is explained in the [Using the Internal](#page-41-1) [Common-Mode Resistor](#page-41-1) section.

Using the Internal Common-Mode Resistor

These devices contain an adjustable internal common-mode resistor, which can be used to increase the dc bias of the DAC outputs. By default, the common-mode resistor is not connected. When enabled, it can be adjusted from ~60 Ω to \sim 260 Ω . Each main DAC has an independent adjustment using the lower six bits in Register 0x05 (IRCML[5:0]) and Register 0x08 (QRCML[5:0]).

Figure 87. Typical CML Resistor Value vs. Register Code

Using the CMLx Pins for Optimal Performance

The CMLx pins also serve to change the DAC bias voltages in the parts allowing them to run at higher dc output bias voltages. When running the bias voltage below 0.9 V and an AVDD of 3.3 V, the parts perform optimally when the CMLx pins are tied to ground. When the dc bias increases above 0.9 V, set the CMLx pins at 0.5 V for optimal performance. The maximum dc bias on the DAC output should be kept at or below 1.2 V when the supply is 3.3 V. When the supply is 1.8 V, keep the dc bias close to 0 V and connect the CMLx pins directly to ground.

APPLICATIONS INFORMATION **OUTPUT CONFIGURATIONS**

The following sections illustrate some typical output configurations for the AD9114/AD9115/AD9116/AD9117. Unless otherwise noted, it is assumed that I_{OUTFS} is set to a nominal 20 mA. For applications requiring the optimum dynamic performance, a differential output configuration is suggested. A differential output configuration can consist of either an RF transformer or a differential op amp configuration. The transformer configuration provides the optimum high frequency performance and is recommended for any application that allows ac coupling. The differential op amp configuration is suitable for applications requiring dc coupling, signal gain, and/or a low output impedance.

A single-ended output is suitable for applications where low cost and low power consumption are primary concerns.

DIFFERENTIAL COUPLING USING A TRANSFORMER

An RF transformer can be used to perform a differential-tosingle-ended signal conversion, as shown in [Figure 88](#page-42-3). The distortion performance of a transformer typically exceeds that available from standard op amps, particularly at higher frequencies. Transformer coupling provides excellent rejection of common-mode distortion (that is, even-order harmonics) over a wide frequency range. It also provides electrical isolation and can deliver voltage gain without adding noise. Transformers with different impedance ratios can also be used for impedance matching purposes. The main disadvantages of transformer coupling are low frequency roll-off, lack-of-power gain, and high output impedance.

Figure 88. Differential Output Using a Transformer

The center tap on the primary side of the transformer must be connected to a voltage that keeps the voltages on IOUTP and IOUTN within the output common-mode voltage range of the device. Note that the dc component of the DAC output current is equal to I_{OUTFS} and flows out of both IOUTP and IOUTN. The center tap of the transformer should provide a path for this dc current. In most applications, AGND provides the most convenient voltage for the transformer center tap. The complementary voltages appearing at IOUTP and IOUTN (that is, VIOUTP and VIOUTN) swing symmetrically around AGND and should be maintained with the specified output compliance range of the AD9114/AD9115/AD9116/AD9117.

A differential resistor, RDIFF, can be inserted in applications where the output of the transformer is connected to the load, R_{LOAD}, via a passive reconstruction filter or cable. R_{DIFF}, as reflected by the transformer, is chosen to provide a source termination that results in a low VSWR. Note that approximately half the signal power is dissipated across RDIFF.

SINGLE-ENDED BUFFERED OUTPUT USING AN OP AMP

An op amp such as the [ADA4899-1](http://www.analog.com/ADA4899-1) can be used to perform a single-ended current-to-voltage conversion, as shown in [Figure 89](#page-42-4). The AD9114/AD9115/AD9116/AD9117 are configured with a pair of series resistors, Rs, off each output. For best distortion performance, R_s should be set to 0 Ω . The feedback resistor, R_{FB}, determines the peak-to-peak signal swing by the formula

$$
V_{\text{OUT}} = R_{\text{FB}} \times I_{\text{FS}}
$$

The common-mode voltage of the output is determined by the formula

$$
V_{CM} = V_{REF} \times \left(1 + \frac{R_{FB}}{R_B}\right) - \frac{R_{FB} \times I_{FS}}{2}
$$

The maximum and minimum voltages out of the amplifier are, respectively,

$$
V_{MAX} = V_{REF} \times \left(1 + \frac{R_{FB}}{R_B}\right)
$$

$$
V_{MIN} = V_{MAX} - I_{FS} \times R_{FB}
$$

Figure 89. Single-Supply Single-Ended Buffer

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DIFFERENTIAL BUFFERED OUTPUT USING AN OP AMP

A dual op amp (see the circuit shown in [Figure 90](#page-43-2)) can be used in a differential version of the single-ended buffer shown in [Figure 89](#page-42-4). The same R-C network is used to form a one-pole differential, low-pass filter to isolate the op amp inputs from the high frequency images produced by the DAC outputs. The feedback resistors, R_{FB}, determine the differential peakto-peak signal swing by the formula

 $V_{OUT} = 2 \times R_{FB} \times I_{FS}$

The maximum and minimum single-ended voltages out of the amplifier are, respectively,

$$
V_{MAX} = V_{REF} \times \left(1 + \frac{R_{FB}}{R_B}\right)
$$

 $V_{MIN} = V_{MAX} - R_{FB} \times I_{FS}$

The common-mode voltage of the differential output is determined by the formula

Figure 90. Single-Supply Differential Buffer

AUXILIARY DACs

The DACs of the AD9114/AD9115/AD9116/AD9117 feature two versatile and independent 10-bit auxiliary DACs suitable for dc offset correction and similar tasks.

Because the AUXDACs are driven through the SPI port, they should never be used in timing-critical applications, such as inside analog feedback loops.

To keep the pin count reasonable, these auxiliary DACs each share a pin with the corresponding FSADJx resistor. They are, therefore, usable only when enabled and when that DAC is operated on its internal full-scale resistors. A simple I-to-V converter is implemented on chip with selectable shunt resistors (3.2 k Ω to 16 k Ω) such that if REFIO is set to exactly 1 V, REFIO/2 equals 0.5 V and the following equation describes the no load output voltage:

$$
V_{OUT} = 0.5 \text{ V} - \left(I_{DAC} - \frac{1.5}{R_s}\right)16 \text{ k}\Omega
$$

[Figure 91](#page-43-3) illustrates the function of all the SPI bits controlling these DACs with the exception of the QAUXEN and IAUXEN bits and gating to prohibit $R_s < 3.2$ k Ω .

Figure 91. AUXDAC Simplified Circuit Diagram

The SPI speed limits the update rate of the auxiliary DACs. The data is inverted such that IAUXDAC is full scale at 0x000 and zero at 0x1FF, as shown in [Figure 92](#page-43-4).

Figure 92. AUXDAC Op Amp Output vs. Current, AVDD = 3.3 V No Load, AUXDAC 0x1FF to 0x000

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Two registers are assigned to each DAC with 10 bits for the actual DAC current to be generated, a 3-bit offset (and gain) adjustment, a 2-bit current range adjustment, and an enable/ disable bit. Setting the QAUXOFS and IAUXOFS bits to all 1s disables the op amp and routes the DAC current directly to their respective FSADJI/ AUXI or FSADJQ/AUXQ pins. This is especially useful where the loads to be driven are beyond the limited capability of the on-chip amplifier. The respective DAC output open circuits when not enabled (QAUXEN or $IAUXEN = 0$).

DAC-TO-MODULATOR INTERFACING

The auxiliary DACs can be used for local oscillator (LO) cancellation when the DAC output is followed by a quadrature modulator. This LO feedthrough is caused by the input referred dc offset voltage of the quadrature modulator (and the DAC output offset voltage mismatch) and can degrade system performance. Typical DAC-to-quadrature modulator interfaces are shown in [Figure 93](#page-44-1) and [Figure 94](#page-44-2). The input common-mode voltage for the modulator could be higher than the output compliance range of the DAC, even with the R_{CM} feature so that ac coupling or a dc level shift is necessary. If the required common-mode input voltage on the quadrature modulator is within that of the DAC, the dc blocking capacitors in [Figure 93](#page-44-1) can be removed. The 50 Ω resistors can, of course be omitted, if the internal resistors are used. A low-pass or band-pass passive filter is recommended when spurious signals from the DAC (distortion and DAC images) at the quadrature modulator inputs can affect the system performance. Placing the filter at the location shown in [Figure 93](#page-44-1) and [Figure 94](#page-44-2) allows easy design of the filter because the source and load impedances can easily be designed close to 50 Ω for a 20 mA full-scale output.

Figure 93. Typical Use of Auxiliary DACs

AD9114/AD9115/AD9116/AD9117

Figure 94. Typical Use of Auxiliary DACs When DC Coupling to Quadrature Modulator ADL537x Family

CORRECTING FOR NONIDEAL PERFORMANCE OF QUADRATURE MODULATORS ON THE IF-TO-RF CONVERSION

Analog quadrature modulators make it very easy to realize single sideband radios. However, there are several nonideal aspects of quadrature modulator performance. Among these analog degradations are gain mismatch and LO feedthrough.

Gain Mismatch

The gain in the real and imaginary signal paths of the quadrature modulator may not be matched perfectly. This leads to less than optimal image rejection because the cancellation of the negative frequency image is less than perfect.

LO Feedthrough

The quadrature modulator has a finite dc referred offset, as well as coupling from its LO port to the signal inputs. These can lead to a significant spectral spur at the frequency of the Quadrature Modulator LO.

The AD9114/AD9115/AD9116/AD9117 have the capability to correct for both of these analog degradations. However, understand that these degradations drift over temperature; therefore, if close to optimal single sideband performance is desired, a scheme for sensing these degradations over temperature and correcting them may be necessary.

I/Q CHANNEL GAIN MATCHING

Fine gain matching is achieved by adjusting the values in the DAC fine gain adjustment registers. For the I DAC, these values are in the I DAC gain register (Register 0x03). For the Q DAC, these values are in the Q DAC gain register (Register 0x06). These are 6-bit values that cover ±2% of full scale. To perform gain compensation by starting from the default values of zero, raise the value of one of these registers a few steps until it can be determined if the amplitude of the unwanted image is increased or decreased. If the unwanted image increased in amplitude, remove the step and try the same adjustment on the other DAC control register. Iterate register changes until the rejection cannot be improved further. If the fine gain adjustment range is not sufficient to find a null (that is, the register goes full scale with no null apparent) adjust the course gain settings of the two DACs accordingly and try again. Variations on this simple method are possible.

Note that LO feedthrough compensation is independent of phase compensation. However, gain compensation could affect the LO compensation because the gain compensation may change the common-mode level of the signal. The dc offset of some modulators is common-mode level dependent. Therefore, it is recommended that the gain adjustment be performed prior to LO compensation.

LO FEEDTHROUGH COMPENSATION

To achieve LO feedthrough compensation in a circuit, each output of the two AUXDACs must be connected through a 10 kΩ resistor to one side of the differential DAC output. See the [Auxiliary DAC](#page-43-5)s section for details of how to use AUXDACs. The purpose of these connections is to drive a very small amount of current into the nodes at the quadrature modulator inputs, therefore adding a slight dc bias to one or the other of the quadrature modulator signal inputs.

To achieve LO feedthrough compensation, the user should start with the default conditions of the AUXDAC registers, then increment the magnitude of one or the other AUXDAC output voltages. While this is being done, the amplitude of the LO feedthrough at the quadrature modulator output should be sensed. If the LO feedthrough amplitude increases, try either decreasing the output voltage of the AUXDAC being adjusted, or try adjusting the output voltage of the other AUXDAC. It may take practice before an effective algorithm is achieved. Using the AD9114/AD9115/AD9116/AD9117 evaluation board, the LO feedthrough can typically be adjusted down to the noise floor, although this is not stable over temperature.

RESULTS OF GAIN AND OFFSET CORRECTION

The results of gain and offset correction can be seen in [Figure 95](#page-45-1) and [Figure 96.](#page-45-2) [Figure 95](#page-45-1) shows the output spectrum of the quadrature demodulator before gain and offset correction. [Figure 96](#page-45-2) shows the output spectrum after correction. The LO feedthrough spur at 450 MHz has been suppressed to the noise level. This result can be achieved by applying the correction, but the correction needs to be repeated after a large change in temperature.

Note that gain matching improves the negative frequency image rejection, but it is also related to the phase mismatch in the quadrature modulator. It can be improved by adjusting the relative phase between the two quadrature signals at the digital side or properly designing the low-pass filter between the DACs and quadrature modulators. Phase mismatch is frequency dependent, so routines have to be developed to adjust it if wideband signals are desired.

Figure 96. AD9114/AD9115/AD9116/AD9117 and ADL5370 with a Single-Tone Signal at 450 MHz, Gain and LO Compensation Optimized

MODIFYING THE EVALUATION BOARD TO USE THE ADL5370 ON-BOARD QUADRATURE MODULATOR

The evaluation board contains an Analog Devices, Inc., [ADL5370](http://www.analog.com/ADL5370) quadrature modulator. The [AD9114/AD9115/](http://www.analog.com/en/prod/0%2C2877%2CAD9776%2C00.html) [AD9116/AD9117 a](http://www.analog.com/en/prod/0%2C2877%2CAD9776%2C00.html)nd the ADL5370 provide an easy-tointerface DAC/modulator combination that can be easily characterized on the evaluation board. Solderable jumpers can be configured to evaluate the single-ended or differential outputs of the AD9114/ AD9115/AD9116/AD9117. This is the default configuration from the factory and consists of the following population of the components:

- JP55, JP56, JP76, JP82—unsoldered
- R13, R14, R52, R53—unpopulated
- R50, R57, T1, T2—populated

To evaluate the ADL5370 on this board, the population of these same components should be reversed so that they are in the following positions:

- JP55, JP56, JP76, JP82—soldered
- R13, R14, R52, R53—populated
- R50, R57, T1, T2—unpopulated

The AUXDAC outputs can be connected to Test Point TP44 and Test Point TP45 if LO feedthrough compensation is necessary.

OUTLINE DIMENSIONS

Figure 97. 40-Lead Lead Frame Chip Scale Package [LFCSP_VQ] 6 mm \times 6 mm, Very Thin Quad $(CP-40-1)$ Dimensions shown in millimeters

ORDERING GUIDE

 $1 Z =$ RoHS Compliant Part.

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